

**Method for the continuous coating of the inside of an extruded hollow profile**

5 The present invention relates to a method for the continuous coating of the inside of an extruded hollow profile strand. The invention also relates to a device for removing excess coating agent from the chambers of a hollow profile.

10 For certain applications, such as for example the glazing of greenhouses or other humid enclosures, twin-wall sheets made of thermoplastic polymers, on the insides of which a water-spreading coating is applied, are used. For example, EP 0 530 617 A1 describes a 15 method for the continuous coating of the inside of an extruded hollow profile made of thermoplastic polymer. In that method, directly after extrusion, a hollow profile strand is guided on a curved path through a supply of a liquid coating agent. After running 20 through the coating agent, the twin-wall strand is guided upward until the entrained excess of liquid coating agent has partly run back into the supply.

25 One problem of this method is the slow run-off rate of the coating agent. As a result, more coating agent remains in the hollow chambers of the strand than is required for the formation of a uniform film on the inner walls. Such an excess leads to the formation of relatively thick and slow-drying films or else to the 30 formation of flow edges, streaks and so-called "flow noses". As a result, the sheets sawn from the hollow profile are wet.

35 Although the sawn sheets are treated at 60°C in a conditioning oven for the purpose of applying an outer laminating film, this treatment is not adequate to remove excess coating agent. The previous solution was to place the sheet onto a carriage with running wheels,

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which tips the sheet in transverse and longitudinal directions, whereby some of the remaining liquid runs off.

5 Since the remaining residue of liquid is still very great, the sheets are subsequently connected to a hot-air fan, it being possible for the sheets to be dried individually in a discontinuous process. With the usual amounts of coating liquid, after this process  
10 crystalline deposits remain in the hollow profile, occurring as white spots, especially on both end faces of the sheet. To remove these remains, 300 mm must be sawn off on both sides of the sheet and form waste material.

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Sawdust produced as a result must in turn be removed from the sheet. This step negates the advantages of the previously performed non-cutting operation of severing after scoring. It is also disadvantageous  
20 that remains of liquid or crystalline deposits get under the previously applied laminating film on the outer sides of the sheets and cause it to come away.

An amount of liquid coating agent inside the sheet in  
25 excess of the amount required for the formation of a uniform film therefore has the result that the continuous extrusion and coating process has to be followed by discontinuous, laborious reworking steps and that reject fabrication with 6-10% material wastage  
30 has to be accepted.

US 5,681,390 describes a spray booth for the spray coating of objects, the inner walls of which are cleaned of finely distributed material by wiping bars.  
35 The wiping bars on the inner walls are moved from the outside by means of magnets.

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Similar systems are used as magnetic window cleaners for aquariums. In those systems, a cleaning magnet on the inside is guided along the window by means of a magnet on the outside, whereby the inside is cleaned.

5 However, the known techniques do not involve continuous methods. The principle of wiping off the contaminants is based on the idea that the wiper is moved while the location on the workpiece that is to be worked is stationary. Moreover, they are only suitable for the 10 removal of solid remains and do not offer a solution for the removal and recovery of excess liquid remains.

In view of the problems of the prior art specified and discussed above, an object of the present invention was 15 to provide a method for coating the inside of a continuously extruded hollow profile strand which can be carried out largely continuously. The previously described discontinuous reworking steps that are made necessary by the remaining excess coating agent were to 20 be reduced.

An object of the invention was also to provide a method with which the offcuts from the hollow profile caused by visible or crystalline coating remains can be 25 avoided as far as possible.

Similarly, the greatest possible proportion of excess coating agent was to be recovered by the method according to the invention. In the case of the 30 previous technique, large amounts of the coating agent occur as waste with the offcuts from the hollow profile and cannot be recovered.

These objects and others which, though not specifically 35 stated, can be deduced as self-evident from the matters discussed herein, or inevitably arise from them, are achieved by a method as claimed in claim 1.

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Expedient modifications of the method according to the invention are afforded protection in the subclaims related back to claim 1, claims 2 to 11. Claims 12 and 5 13 relate to a liquid wiper and a device for removing excess coating agent from the chambers of a hollow profile, with which the method according to the invention can be carried out.

Drawing 1 shows a preferred embodiment of a liquid wiper as used in the method according to the invention. 10 In drawing 2, a device for carrying out the method according to the invention is represented schematically in a vertical sectional image. Drawing 3 shows the preferred embodiment of a produced hollow profile 15 strand in a cross-sectional view. Drawing 4 shows a liquid wiper as it is mounted in a hollow chamber.

The fact that excess coating agent is wiped from the inner walls by liquid wipers mounted inside the hollow 20 chambers, by the hollow profile strand being moved continuously in relation to the liquid wipers, the liquid wipers, which comprise at least one magnet or magnetizable material and a wiping lip that touches the inner walls and are arranged in the region of the rise 25 in the path of the hollow profile downstream of the supply of coating agent, being securely held at a constant position within the path of the hollow profile strand by counter magnets or magnetizable materials, which are fixed next to the outer side of the 30 continuous hollow profile strand, accomplishes the effect that the coating of the inside of the hollow profile strand can be carried out continuously and the discontinuous subsequent treatment steps described in the prior art for the removal of excess coating agent 35 can be eliminated.

Furthermore, visible or crystalline coating remains in the hollow chambers after drying, and offcuts from the hollow profile produced as a result, are avoided.

5 By the method according to the invention it is also possible to reduce the consumption of liquid coating agent appreciably. For instance, the consumption is merely one twelfth of the consumption in the method according to EP 0 530 617 A1. This is equivalent to  
10 saying that the supply of coating agent lasts twelve times longer in comparison with the method given there.

The method according to the invention is described below in one particular embodiment, without any  
15 restriction being intended as a result.

In the first step, in an extrusion system, including an extruder, an extrusion slot die and a cooled calibrator, a hollow profile strand is continuously  
20 drawn off at a uniform rate after cooling, in the case of plastics preferably to below the glass transition temperature.

For the purposes of the invention, hollow profile  
25 strands are taken as meaning extruded strands with a constant profile which contain at least one continuous hollow space. These include pipes and frame profiles, glazing-bar profiles and other technical profiles with more or less complicated cross-sectional shapes and, if  
30 appropriate, a number of hollow spaces. The wall thickness of the layer enclosing the hollow space is generally 0.1 to 5 mm. A precondition for processability by the method of the invention is an elastic flexibility of the extruded hollow profile in  
35 the direction of extrusion, which in the case of plastics, for example, allows bending radii of approximately 1 to 100 m, at least at temperatures lying just below the glass transition temperature.

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Such flexibility is generally obtained if the hollow profile is not thicker than 40 mm.

Preferably, twin-wall sheets are produced and coated.

5 Drawing 4 shows the preferred form of a hollow profile strand as produced by the method according to the invention in a cross-sectional view.

10 All elastic materials which allow the necessary bending, as well as thermoplastically extrudable polymers with a modulus of elasticity of at least 1000 MPa, measured at 200°C to DIN 53457, preferably 1500 to 4000 MPa, are suitable for the method of the invention.

15 Their glass transition temperature (DIN 7724) is at least 50°C, preferably 70 to 200°C. Typical construction plastics for the building trade, which are distinguished by hardness and rigidity and also by resistance to weathering effects, are preferred. For example, polymethyl (meth)acrylates, polycarbonates, 20 polyvinyl chloride, polystyrene, ABS, unvulcanized rubbers, silicones, vulcanized rubber, cork, glass-fiber reinforced or carbon-fiber reinforced plastics and metals are preferred. The notation (meth)acrylate means here both methacrylate, such as for example 25 methyl methacrylate, ethyl methacrylate etc., and acrylate, as well as mixtures of the two.

30 Polymethyl (meth)acrylates are generally obtained by radical polymerization of mixtures which contain methyl (meth)acrylate. These mixtures generally contain at least 40% by weight of methyl (meth)acrylate, preferably at least 60% by weight and with particular preference at least 80% by weight, in relation to the weight of the monomers.

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Comonomers may also be used. The comonomers are generally used in an amount of 0 to 60% by weight, preferably 0 to 40% by weight and with particular

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preference 0 to 20% by weight, in relation to the weight of the monomers, it being possible for the compounds to be used individually or as a mixture.

5 The poly (meth)acrylate may comprise further polymers to modify the properties. These include, inter alia, polyacrylonitriles, polystyrenes, polyethers, polyesters, polycarbonates and polyvinyl chlorides. These polymers may be used individually or as a  
10 mixture, it also being possible to use copolymers which can be derived from the aforementioned polymers.

The thermoplastic polymers for the production of the hollow profile strand may contain customary  
15 additives/additions of all kinds. These include, inter alia, dyes, antistatic agents, antioxidants, mold release agents, flame retardants, lubricants, flow improvers, fillers, light stabilizers and organic phosphorus compounds, such as phosphites or  
20 phosphonates, pigments, antiweathering agents and plasticizers.

According to one particular aspect of the present invention, the thermoplastic polymer may, if appropriate, be made mechanically more stable by  
25 incorporating an impact modifier.

This is the case in particular if poly(meth)acrylates or polycarbonates are used.

30 As it runs through the extrusion system, the hollow profile strand of elastic material, with preference of thermoplastic polymer, is guided under elastic flexure through a downwardly curved arcuate path. Firstly, the  
35 strand is guided downward, the maximum angle of drop, measured in relation to the horizontal, preferably being between 3° and 20°, in particular between 5° and 10°. After passing the lower vertex, the hollow

profile strand is guided upward, preferably rising at an angle, measured in relation to the horizontal, of at most 3° to 20° and in particular at an angle of 5° to 10°. Following the rise, the strand can again be 5 guided substantially horizontally for cooling, preferably as far as a cutting device, where it is divided into portions or twin-wall sheets of a desired length.

10 The difference in height between the extrusion die and the lower vertex of the path is preferably between 200 mm and 600 mm, with particular preference 350-450 mm. The difference in height between the lower vertex and the horizontal portion of the path following 15 the rise is preferably between 200 mm and 600 mm, with particular preference 300 mm - 400 mm. Accordingly, the radius of curvature of the path is between 4000 mm and 26,000 mm. The advancing rate of the hollow profile strand is generally between 0.2 and 2.5 m/min 20 and preferably between 0.5 and 1.5 m/min.

In the region of the lower vertex of the path, there is in the hollow chambers a supply of liquid coating agent which remains stationary in its location. It is always 25 kept up to an amount great enough for the liquid level to touch the inside of all the walls of the hollow chamber.

The coating agent is first filled into the hollow 30 chamber once a sufficiently long piece of the hollow profiled sheet has been extruded and guided through the path. Normally, one filling is sufficient for an operating period of several hours to days.

35 The advantageousness of an inside coating arises from the respective application area of the hollow profile. For example, it was proposed in EP-B 201 816 to provide a twin-wall sheet of plastic on the outside and inside

with a coating of a lower optical refractive index than that of the plastic. As a result, reflection losses of the light passing through are reduced and the overall light transmission is increased.

5 A preferred application of the method according to the invention is that of applying a water-spreading coating to the inside surfaces of twin-wall sheets. The necessity for such a coating arises in the case of glazings of greenhouses and other humid enclosures.

10 Coating agents for this purpose are known for example from EP-B 149 182.

However, it must not go unmentioned that it is also possible by means of the invention, if required, for a 15 number of layers to be applied one after the other by the twin-wall sheet being passed through a number of coating zones designed in the way provided by the invention one after the other. A precondition is that the first coating can be cured before the sheet enters 20 the second coating zone. In this way it is possible, for example, for an adhesion-promoting primer to be created for the second coating.

Low-viscosity coating agents with a viscosity in the range from 1 to 4000 mPas, preferably 2 to 25 mPas, are 25 generally used for the method of the invention, it being possible to add solvents to the coating agent. In principle, high-viscosity coating agents can also be used.

30 What is important is satisfactory wetting of the surface of the plastic by the liquid coating agent, so that a continuous film is formed. If this is not the case, a wetting agent may be added. In most cases, a physically drying liquid coating agent is used, which 35 comprises a dissolved, dispersed or suspended non-volatile or low-volatility coating agent and a volatile liquid. Water-spreading and optically effective coatings and their production are described in EP

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0530617. Furthermore, all coating agents with suitable viscosity, such as for example oils, paints etc., can be used with the method according to the invention.

- 5 The method of the present invention is characterized in that excess liquid coating agent is wiped from the inner walls of the hollow chambers by liquid wipers which are located inside the hollow chambers.
- 10 For the purposes of the present invention, excess means the amount of coating agent that exceeds the amount required for the continuous formation of a film on the inner walls of the hollow chambers.
- 15 The amount depends, inter alia, on the viscosity of the coating agent, the extrusion rate and the angle at which the strand is advanced. The amount of excess coating agent is generally 5-98% by volume and, in the more specific case, 20-97% by volume of the total 20 amount used.

The wiping takes place by means of the continuous movement of the extruded hollow profile strand or the hollow chamber concerned in relation to the stationary 25 liquid wipers, which in each case comprise at least one wiping lip and a magnet or magnetizable material.

There is preferably a liquid wiper for wiping off excess coating agent in each of the continuously 30 extruded hollow chambers. However, it is not absolutely necessary to arrange a liquid wiper in each hollow chamber. Similarly, it is possible to arrange wipers only in a selection of hollow chambers from which excess coating agent is to be removed.

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Similarly, it is possible to arrange two or more liquid wipers in a single hollow chamber. These may be arranged both next to one another and one behind the

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other and optionally be connected to one another. A number of liquid wipers may be arranged in such a way that they wipe coating agent from different walls of the hollow chamber.

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The wiping lip of each liquid wiper is arranged in such a way that it touches one or more inner walls of the hollow chamber. Excess liquid is wiped from the inner walls which are touched by the wiping lip by the 10 extruded hollow profile strand being advanced continuously on its path.

Suitable in principle as materials for the wiping lip are those which are chemically resistant to the coating 15 agent, have low friction, in order to provide uniform advancement of the liquid wiper, are adaptable to the shape of the twin-wall profile and at the same time are elastic enough for the adaptation to a changed chamber profile to be possible.

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The wiping lip preferably consists of Teflon or silicone. Expanded Teflon, which has a density of between 0.3 and 1.8 g/cm<sup>3</sup>, is particularly suitable. Furthermore, a silicone tube is particularly suitable 25 as the material for the wiping lip.

During the wiping, the liquid wiper and the wiping lip are kept stationary in their location by the interaction between a magnet and a counter magnet or 30 magnetizable materials, while the twin-wall strand moves. The magnet or magnetizable body is part of the liquid wiper and is likewise located inside the hollow chamber.

35 At least one magnet, counter magnet or magnetizable body per liquid wiper is fixed next to the outer side of the continuous hollow profile strand and keeps the liquid wiper in a substantially constant position

within the path of the hollow profile strand. The liquid wiper inside the hollow profile strand is kept in its position by the magnet, counter magnet or magnetizable body outside the strand without touching 5 it. The magnet, counter magnet or magnetizable body is preferably fixed next to the hollow profile strand in such a way that the distance between the surface of the magnet and the outer side of the strand is between 2 mm and 10 mm. Furthermore, magnets, counter magnets or 10 magnetizable bodies may be fixed opposite one another on both sides of the hollow profile strand and keep a liquid wiper stationary in its location.

15 The geometry of the magnets, counter magnets or magnetizable bodies is appropriately made to match the geometry of the hollow profile. If a hollow profiled sheet is produced, as shown Figure 3, flat magnets are preferably used, the flat surfaces of which are aligned in the longitudinal and transverse directions parallel 20 to the outer walls of the continuous strand.

The magnets are selected in dependence on the friction coefficients of the liquid. Suitable for the use according to the invention are magnets which have an 25 energy density of between 200 and 380 kJ/m<sup>3</sup>. A precondition is a magnetic field which is strong enough for the counter magnet or magnetizable body to keep the liquid wiper in its position during the movement of the hollow profile strand. In this case, the hollow 30 profile strand preferably moves at a rate of 0.5-2.5 m/min. Preferably used as magnets and counter magnets are Nd-Fe-B magnets, which have an energy density that is 10 to 12 times higher than conventional iron magnets. Apart from neodymium-iron-boron magnets, 35 in principle any other magnets that have a comparable energy density can also be used. In this case, electromagnets can also be used. Instead of magnets, magnetizable materials in combination with permanent

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magnets or electromagnets are suitable for the method according to the invention.

5 Liquid wipers and counter magnets or magnetizable bodies are located in the region of the rise of the path of the hollow profile following the supply of coating agent. The rise in this portion of the path is preferably between 5° and 10°.

10 Liquid wipers and counter magnets or magnetizable bodies are stationary in their location with respect to the supply of coating agent and the extrusion system during the method, while the hollow profile strand is continuously in motion. The arrangement in the region of the rise of the path has the effect that the wiped coating agent flows back into the supply of coating 15 agent and is available for the further coating process.

20 In a preferred embodiment of the method, a liquid wiper which comprises not only the described wiping lip and the magnet but also a lip of a material which can be impregnated with the coating agent is used.

25 Such a lip is located downstream of the wiping lip in the direction of the path of the hollow profile strand and, like said wiping lip, touches one or more inner walls of the hollow chamber. During the process sequence, the lip is impregnated with liquid coating agent and therefore brings about a particularly uniform distribution of the coating agent on the inner walls of the hollow chamber.

30 Similarly, the lip impregnated with coating liquid brings about the continuous formation of a coating film on the inner walls of the hollow chamber, if at points of the inner walls the coating agent is completely 35 wiped off by the wiping lip.

A preferred material for the liquid-impregnatable lip is felt. Similarly suitable in principle for such a

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lip are all other liquid-impregnatable materials, such as for example sponges and woven fabrics, that are substantially chemically resistant to the coating agent, have a low friction, in order to provide uniform 5 motionlessness of the liquid wiper, are adaptable to the shape of the twin-wall profile and at the same time are elastic enough for the adaptation to a changed chamber profile nevertheless to be possible.

10 In principle, a liquid wiper which only comprises the magnet, counter magnet or magnetizable material and the wiping lip can be used. In this case, the magnet, counter magnet or magnetizable material itself forms the body of the liquid wiper, to which the wiping lip 15 is fastened. Used with preference, however, is a liquid wiper which is formed by a non-magnetic body to which the magnet, counter magnet or magnetizable material, the wiping lip and, if appropriate, also a liquid-impregnatable lip are fastened.

20 The non-magnetic body of the liquid wiper may in principle consist of a material that is substantially inert to the coating agent. Preferred materials are plastics such as poly(meth)acrylate, polystyrene, 25 polycarbonate.

In one embodiment, the method according to the invention is devised in such a way that the inner wall of the hollow chamber is touched exclusively by one or 30 more wiping lips and, if appropriate, additionally by a liquid-impregnatable lip. This is achieved by the lips that are present projecting beyond the magnet or magnetizable material or the body of the wiper.

35 The magnet, counter magnet or magnetizable material of the liquid wiper and of the possibly present non-magnetic bodies do not touch the inner walls, since a mechanical effect of these components on the inner wall

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is undesired because of the possible damage to the coating film.

In a further preferred embodiment, a liquid wiper which  
5 has one or more rotatable rollers fastened to its magnetic or non-magnetic body is used. The liquid wiper is mounted in the hollow chamber by means of these rollers. The rollers are arranged in such a way that, as a result of the force of attraction of the  
10 magnet or counter magnet, they touch at least the wall of the hollow profile strand that is located between the magnet, counter magnet or magnetizable material of the liquid wiper and the counter magnet. Similarly, however, further inner walls may also be touched by  
15 rollers on the liquid wiper.

The rollers may, in principle, consist of any material that is substantially inert to the coating agent. Preferred are plastics, such as for example  
20 poly(meth)acrylate, polycarbonate, polystyrene or polyamide.

As a result, the liquid wiper according to the previously described embodiment touches one or more inner walls of the hollow chamber not only with the  
25 wiping lip and the possibly present liquid-impregnatable lip but also with the rollers. When there is movement of the hollow profile strand, the rollers are set in rotation.

30 The rollers act as spacers between the wall of the hollow profiled chamber and the magnet, counter magnet or magnetizable material and the body of the liquid wiper. The defined distance makes it possible to achieve a particularly uniform contact pressure of the  
35 wiping lips against the wall and particularly uniform wiping.

By the method described, continuous films are formed on the inner walls of the hollow chamber, the film thickness of which in the moist state is generally between 0.05  $\mu\text{m}$  and 3000  $\mu\text{m}$  and preferably between 5 2.5  $\mu\text{m}$  and 3.0  $\mu\text{m}$ . After drying of the coating agent, the film thickness is generally between 50 nm and 300 nm and preferably between 60 nm and 160 nm.

10 The resulting film thickness is dependent on a large number of parameters, some of which are mentioned hereafter. For example, the force of attraction between the liquid wiper and the magnet, magnetizable body or counter magnet plays a role in determining the contact pressure of the wiping lip against the hollow 15 chamber wall.

Similarly, the film thickness and the uniformity of the film depend on which friction, elasticity and adaptability to the shape of the hollow profile the 20 material of the wiping lip has. Furthermore, the film thickness is determined by the density of the felt which is used for the felt lip.

If the body of the liquid wiper is provided with 25 rollers, the distance defined by the rollers from the body to the hollow chamber wall and the maximum compression of the wiping lips defined thereby are of significance for the film thickness.

30 The invention likewise relates to a liquid wiper, and a device for removing excess coating agent. These are represented in one particular embodiment on the basis of drawings 1-4, without intending to restrict the invention to this embodiment.

35 The liquid wiper shown in drawing 1 comprises a body (1), to which two magnets, counter magnets or magnetizable materials (2) are fastened in recesses

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(3). Similarly, at least one wiping lip (4) and a felt lip (5) are fastened to the body. Rollers (6) are mounted on spindles (7) in further recesses of the body.

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The preferred embodiment of a device for carrying out the method according to the invention is shown in drawing 2. Arranged after an extrusion device (not represented here) are guiding rollers (21-29), which direct an extruded hollow profile strand (8) onto a downwardly curved arcuate path. In the dip of the path there is a supply of coating agent (9) in the hollow chambers of the strand. Arranged in each of the hollow chambers of the strand are two liquid wipers (10a, 10b). Drawing 2 shows only one of the hollow chambers in longitudinal section with two liquid wipers arranged therein. Next to the outer sides of the hollow profile strand or the hollow chamber, magnets, counter magnets or magnetizable bodies (11) are fastened to holding devices (12). Liquid wipers, counter magnets, magnets or magnetizable bodies and holding devices are arranged in the rising portion of the path of the hollow profile after the supply of coating agent.

25 After the rollers (28, 29), the path of the hollow profile runs horizontally. In the horizontal portion, a cutting device (not shown in drawing 2) for dividing the hollow profile strand into portions or twin-wall sheets of a desired length is arranged.

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Drawing 3 shows the cross section of the hollow profile, which in drawing 2 is represented in longitudinal section. It is a twin-wall sheet, in which a hollow chamber (16) is bounded by two flanges (17, 18) and two webs (19, 20). The two liquid wipers (10a, 10b) respectively lie with their rollers and lips only on one of the flanges, as shown in drawing 2, and with their lips touch the flange and part of the webs.

Therefore, as shown in drawing 2, two liquid wipers (10a and 10b) are arranged in each hollow chamber (16), the first liquid wiper touching with its lips the upper flange (17) and the upper part of the webs (19, 20) and the second liquid wiper touching with its lips the lower flange (18) and the lower part of the webs (19, 20). The first liquid wiper (10a) is located upstream of the second liquid wiper (10b) in the direction of the path (L) of the hollow profile strand. The two liquid wipers can be connected to each other by a flexible connecting part (not shown in drawing 2). The connection is therefore flexible, because the hollow profiled sheet is curved in the region of the rise in which both liquid wipers are located and the angle of the rise in relation to the horizontal varies preferably between about 6° and 9°.

Drawing 4 shows the liquid wiper (10b) according to drawing 1 and drawing 2 in longitudinal section, resting with its rollers (6) and its lips (4, 5) on the lower flange (18) of a hollow chamber.

The way in which the devices and components described above from drawings 1-4 function in the method according to the invention is described below.

In a first step, a hollow profile strand is extruded from the extrusion die at a rate of preferably between 30 0.2 and 5.0 m/min. The strand emerging from the die is guided through between the rollers (21) and (22) and subsequently directed by means of elastic flexure under the lowermost roller (23). After the roller (23), the strand is guided through under elastic flexure between 35 the rollers (24)/(25) and (26)/(27). Finally, the strand is guided through, once again under elastic flexure, between the rollers (28) and (29). The arrangement of the guiding rollers produces an arcuate

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path of the strand. The roller (23) at the lower vertex of the path acts against the elastic resilience of the strand.

5 In the region of the lower vertex of the path, there is in the hollow chambers a supply of a liquid coating agent which remains stationary in its location. It is always kept up to an amount great enough for the liquid level to touch the inside of all the walls of the  
10 hollow chamber.

By means of a slide, preferably of an optical-fiber cable, two liquid wipers (10a, 10b) are then pushed into each of the hollow chambers one after the other  
15 until they are positioned next to the magnets, counter magnets or magnetizable bodies (11) and are kept stationary by the latter.

After emerging from the extrusion die, the continuously  
20 advancing strand firstly runs through the supply of liquid coating agent in the dip of the arcuate path, whereby the inner walls of the hollow chambers (16) are wetted with coating agent. Subsequently, the strand moves past the first liquid wipers (10a), which wipe  
25 excess coating agent from the upper flange (17) and upper part of the webs (19, 20) of each hollow chamber (16). Wiped-off coating agent consequently flows or drips onto the lower flange of the hollow chambers and flows partly back into the supply of coating agent.  
30 Excess coating agent which does not flow off quickly enough and collects on the lower flange (18) and the lower part of the webs (19, 20) is subsequently wiped off by the second liquid wiper and can flow back into the supply.

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Once the strand has moved past both liquid wipers, it assumes a substantially horizontal path and can be fed to the cutting device.